POWER INDUCTORS TRANS-INDUCTANCE VOLTAGE REGULATOR (TLVR) INDUCTORS



The Trans-Inductor Voltage Regulator (TLVR) has emerged as a promising topology for powering low-voltage, high-current, multiphase applications such as data centres, storage systems, graphics cards, and personal computing. These systems require a reliable and efficient power delivery solution that can support processors, memory, and high-current ASICs and FPGAs.

Traditionally, voltage regulator modules (VRMs) have been used to meet these requirements. However, the increasing demands of these applications have led to the limitations of the traditional approach. The TLVR circuit was introduced proposing a novel approach that replaces the traditional inductors with transinductors (1:1 ratio transformers). This change dramatically improves transient response and voltage regulation and has been widely adopted in VR14 and related programs. Despite the significant benefits of the TLVR topology, there has been little investigation of the magnetic components' actual performance, efficiency, manufacturability, and cost. This paper aims to address this gap by reviewing both the non-TLVR and TLVR topologies and magnetic structures. Additionally, the paper will examine the circuit waveforms and 3D finite element models and provide a detailed analysis of the trade-offs between the two approaches. The analysis will include an efficiency comparison based on simulation results.

PRI-SEC WINDING

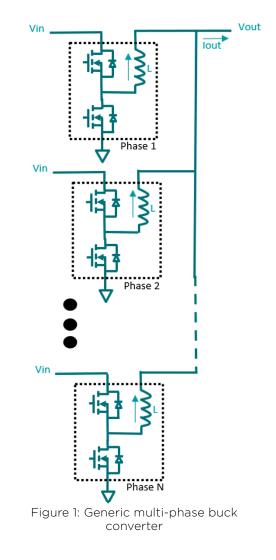


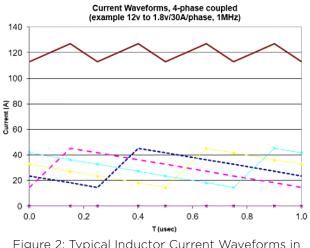
VOLTAGE REGULATOR MODULE (NON TLVR)

Traditional VRMs commonly used in high-current applications like data centres and FPGAs employ a multiphase buck regulator. This regulator typically consists of several tightly packed power stages with 5*6mm or 4*6mm, each with an inductor of around 6x12 mm or 6x10 mm size, and a height of 12 mm. The input voltage in these applications is around 12V, while the output voltage can be as low as 1.X V or 0.8 V.

During normal operation, one phase in the multi-phase buck regulator is turned on, while the others remain off, and continue to cycle through. While each phase will have a ripple current like that of a traditional buck converter, the currents into the output are summed, creating an overall smaller ripple. An example of the inductor current waveforms and output current ripple can be seen in Figure 2.

During a transient period, the current per phase can increase rapidly, leading to a drooping in the output voltage before the converter can respond and regulate properly. This increase in load current can be seen in Figure 3.







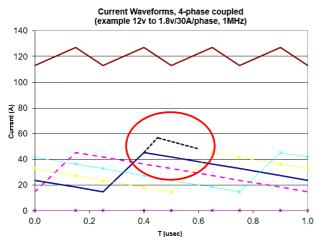


Figure 3: VRM Phase Current Transient

PRI-SEC WINDING



VOLTAGE REGULATOR MODULE (NON TLVR)

As the converter is not able to respond to the change in load current until the next phase switches on, the output voltage will temporarily droop, as seen in Figure 4. In sensitive processor circuits, this output voltage droop can become problematic, and novel converter approaches are needed to support more strict transient responses, especially as processor demands continue to increase.

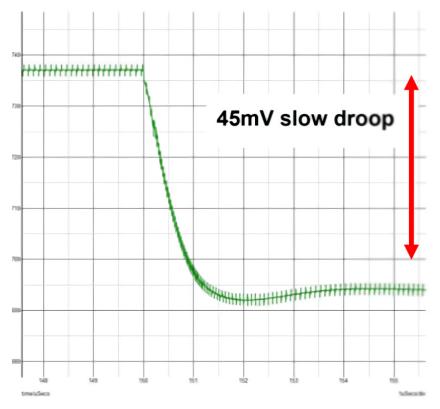


Figure 4: VRM Output Voltage Droop

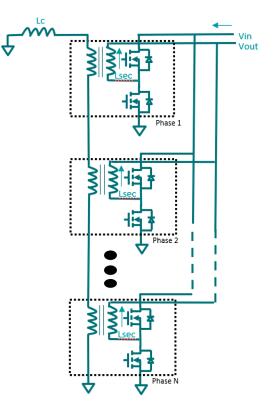
PRI-SEC WINDING

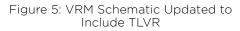


TRANS INDUCTOR VOLTAGE REGULATOR (TLVR)

The TLVR is a novel approach to voltage regulation that maintains the traditional multi-phase buck approach used in VRMs but modifies the inductors by adding an additional 1 turn inner lead, creating a trans-inductor. This modification enables the TLVR to eliminate voltage droop/overshoot during an increase/decrease in current, making it a more efficient voltage regulator.

In a TLVR circuit, all of the newly added primary windings are placed in a series loop, with an external compensation inductor added to fine-tune the transient response. The schematic for a TLVR circuit is almost identical to the traditional VRM, with the only significant difference being the inclusion of the TLVR inductor. Figure 5 shows the updated schematic of the TLVR circuit. During the transient load step/ release, the voltage across the Lcincreases/decreases, which in turn increases/decreases the Lc inductor current. The current through Lc is reflected to the PRIMARY winding of each phase. All phase currents see the same current change. The result is a regulator supplying more to help reduce the output capacitors' discharge, leading to a faster transient response and better voltage overshoot/droop control. The TLVR structure significantly improves transient response and reduces output voltage droop/overshoot compared to traditional VRMs.





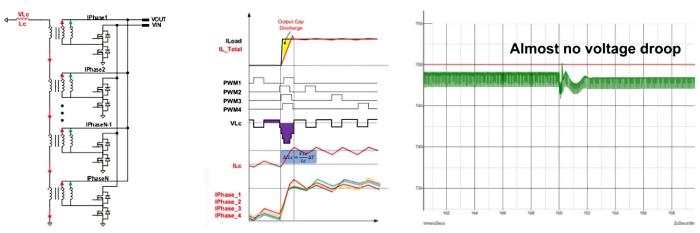


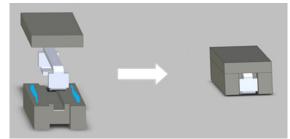
Figure 6: Reduced Output Voltage Droop with TLVR

PRI-SEC WINDING



MAGNETIC STRUCTURE

The magnetic structure of TLVR inductors is very similar to that of traditional inductors used in VRMs. Traditional inductors have a simple construction consisting of two low loss ferrite core halves and a single turn lead. They are available in two varieties – a "U-I" core to minimize height at the expense of footprint and an "E-E" core to minimize footprint at the expense of height.





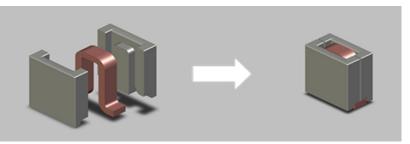


Figure 8: EE core bead for smaller footprint

On the other hand, TLVR inductors utilize the same "E-E" core but have an additional single turn inner lead, which is shown in Figure 9. As a result, the overall layout of the TLVR circuit becomes relatively simple, with the inner leads routed in series with short copper runs, and a traditional VRM layout is used. Existing manufacturing processes can be used for the construction of TLVR inductors, making it a straightforward modification of the existing inductor construction.

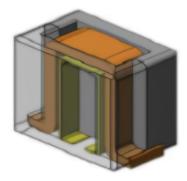




Figure 9: TLVR construction with inner lead

PRI-SEC WINDING



POTENTIAL CHALLENGES AND SOLUTIONS WITH TLVR INDUCTORS

TLVR inductors have shown great promise in revolutionizing power management solutions, thanks to their modified construction that allows for an additional winding resulting in higher efficiency and reduced output capacitor requirements. However, with any new technology, there are potential challenges that need to be addressed in order to fully realize the benefits of TLVR inductors. Three potential challenges that currently face TLVR inductors include mechanical stability, phase-phase isolation voltage, and added cost. Addressing these challenges is crucial for TLVR inductors to become a widely adopted technology.

MECHANICAL STABILITY

One challenge that arises when adding an additional winding to TLVR inductors is the mechanical stability of the inductor. Traditional "EE" core inductors, that are designed for small footprint are typically narrower than their height, making them potentially unstable and prone to placement issues in pick and place operations. TLVR inductors face the same challenge, but with the added complexity of ensuring that the inner and outer leads are coplanar. This requires a careful lead placement process during manufacturing and advanced optical inspection (AOI) to ensure tight coplanarity between the leads. To address this challenge, co-joined inductors can be manufactured to create a wider overall inductor without requiring spacing between inductor phases, thereby minimizing total solution space and increasing component stability. However, further work is needed to validate the performance of this co-joined TLVR construction at the circuit level. Figure 10 illustrates the proposed co-joined TLVR construction.

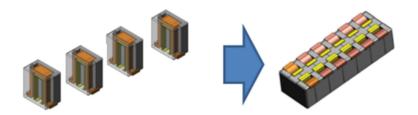


Figure 10: Proposed co-joined TLVR Construction

PRI-SEC WINDING



PHASE - PHASE ISOLATION VOLTAGE

When using TLVR inductors with the primary winding routed in series, a voltage loop is formed, and the voltages from each primary winding will sum around the loop, ultimately leading to a high voltage differential across the isolation barrier. This can create reliability issues, especially for high phase counts and large voltage differentials where the voltages can exceed 100V, as illustrated in Figure 11. While current TLVR constructions place the primary and secondary of each magnetic close together for tighter coupling, it is possible to create high isolation TLVR magnetics with capabilities exceeding 100V by coating the core with non-conductive materials and adding an additional insulation to the winding leads. However, this comes with added costs and reduced winding window within the core.

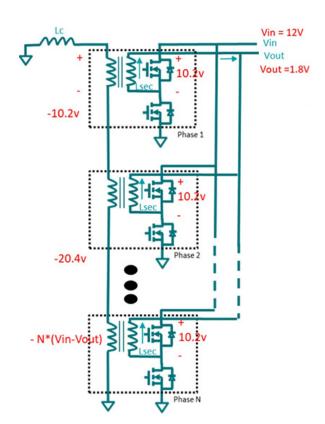


Figure 11: Potential Voltage Differentials across TLVR Windings

INCREASED COSTS

The TLVR magnetic comes with the added complication of lead manufacturing, and potential adders for higher isolation, making it typically 15-50% more expensive than its traditional counterpart, depending on the nuances of the design. However, over time, it is expected that process improvements from individual manufacturers will close the cost gap.

At the converter level, the TLVR solution usually offers modest cost improvements overall due to reduced output capacitor requirements resulting from the reduced ripple.

PRI-SEC WINDING



EFFICIENCY COMPARISONS

Many of the challenges faced in implementing TLVR technology have well-established mitigation strategies in place across the industry. However, the comparison in efficiency at the magnetic level is less highlighted. While traditional VRM inductor losses are well understood, the same loss mechanisms - fringing loss, core loss, and skin depth losses - are still present in the TLVR inductor, along with two added complications. The first complication is the creation of a small amount of proximity loss due to the two windings conducting simultaneously. The more significant issue is that a high-frequency ripple of Nphases*fsw is superimposed on top of the traditional buck inductor waveforms, resulting in excess loss not present in the VRM circuit.

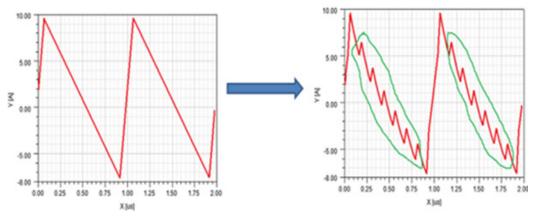


Figure 12: High Frequency Ripple Current From Series Coupled primary Winding

To estimate the added core loss, a first pass approach involves separating the low-frequency buck waveform from the high-frequency ripple and summing the loss. However, this approach has some potential drawbacks, such as core loss not being perfectly linear and depending on having an accurate core loss model for the much higher frequency. Furthermore, the high-frequency content introduces additional AC winding loss via fringing and proximity effects. When simulating similar E-E core constructions with both traditional VR windings and TLVR windings, the winding loss of the TLVR inductor can be as much as 11x higher. To obtain a more accurate understanding of TLVR inductor losses, several gap lengths and frequencies were simulated using commercially available software. These losses are summarized in Appendix A.

Based on these results, further work is needed to develop both lower loss, high-frequency core materials, and novel methods to alleviate AC winding effects such as fringing loss. Although these challenges are not yet fully understood, continued research and development in this area will be crucial for improving TLVR technology and increasing its adoption in the industry.



PRI-SEC WINDING

APPENDIX A								
Dash no.	type	Gap (mm)	Frequency	Delta 1 (A)	Simulated Core Loss (mW Avg)	Simulated Solid Loss (mW Avg)	Simulated Voltage (V rms)	Remark
100nH	Non TLVR	0.165	1MHz	8.5	72.75	29.97	2.7513	
100nH	TLVR	0.165	1MHz	8.5	197.9	195.3	10.4634	290mW higher loss
100nH	Non TLVR	0.165	800KHz	10.625	72.74	36.62	2.752	
100nH	TLVR	0.165	800KHz	10.625	192.9	248.8	10.4703	330mW higher loss
150nH	Non TLVR	0.097	1MHz	8.5	142.1	32.14	4.2644	
150nH	TLVR	0.097	1MHz	8.5	403.8	198.3	8.2522	430mW higher loss
150nH	Non TLVR	0.097	800KHz	10.625	141.7	39.46	4.2611	
150nH	TLVR	0.097	800KHz	10.625	400.6	251.8	8.2467	~470mW higher loss

CONCLUSION

There is no doubt that the TLVR circuit enables a significant improvement in both transient response and voltage regulation during load-step. However, the presentation shows that these circuit advantages create additional losses within the magnetics, require significant constructional complexity and increase the overall cost of the magnetics. In addition, there is a potential, as phase count increases, to have voltage breakdown within the magnetics. All of which need to be considered when implementing a TLVR solution.

AUTHOR BIOGRAPHY

Damon Huang is a Product Manager and Applications Engineer for the Power Business Unit of Pulse responsible for defining, developing, and supporting next generation power magnetics. Prior to Pulse Damon was a power engineer in Telecom Power Supply. Damon currently resides in Suzhou, China.

Yosef Zhou is a Design Specialist for the Power Business Unit of Pulse Electronics. Yosef has over 10yrs of design experience with power magnetic design, simulation and measurement. Yosef currently resides in Zhuhai, China.